## P-I Servoamplifier <br> G122-829A001

## Application Notes

## 1 Scope

These Application Notes are a guide to applying the G122-829A001 P-I Servoamplifier. These Application Notes can be used to:

- Determine the closed loop structure for your application.
- Select the G122-829A001 for your application. Refer also to data sheet G122-829.
- Use these Application Notes to determine your system configuration.
- Draw your wiring diagram.
- Install and commission your system.

Aspects, such as hydraulic design, actuator selection, feedback transducer selection, performance estimation, etc. are not covered by these Application Notes. The G122-202 Application Notes (part no C31015) cover some of these aspects. Moog Application Engineers can provide more detailed assistance, if required.

## 2 Description

The G122-829A001 is a general purpose, user configurable, P-I servoamplifier. Selector switches inside the amplifier enable either proportional control, integral control, or both to be selected. Many aspects of the amplifier's characteristics can be adjusted with front panel pots or selected with internal switches. This enables one amplifier to be used in many different applications. Refer also to data sheet G122-829.

## 3 Installation

### 3.1 Placement

A horizontal DIN rail, mounted on the vertical rear surface of an industrial steel enclosure, is the intended method of mounting. The rail release clip of the G122-829A001 should face down, so the front panel and terminal identifications are readable and so the internal electronics receive a cooling airflow.

An important consideration for the placement of the module is electro magnetic interference (EMI) from other equipment in the enclosure. For instance, VF and AC servo drives can produce high levels of EMI. Always check the EMC compliance of other equipment before placing the G122-829A001 close by.

### 3.2 Cooling

Vents in the top and bottom sides of the G122-829A001 case provide cooling for the electronics inside. These vents should be left clear. It is important to ensure that equipment below does not produce hot exhaust air that heats up the G122-829.


### 3.3 Wiring

The use of crimp "boot lace ferrules" is recommended for the screw terminals. Allow sufficient cable length so the circuit card can be withdrawn from its case with the wires still connected. This enables switch changes on the circuit card to be made while the card is still connected and operating. An extra 100 mm , for cables going outside the enclosure, as well as wires connecting to adjacent DIN rail units, is adequate.

The screw terminals will accommodate wire sizes from $0.2 \mathrm{~mm}^{2}$ to $2.5 \mathrm{~mm}^{2}$ (24AWG to 12AWG). One Amp rated, $0.2 \mathrm{~mm}^{2}$ should be adequate for all applications.


Preferred Wiring


### 3.4 EMC

The G122-829A001 emits radiation well below the level called for in its CE mark test. Therefore, no special precautions are required for suppression of emissions. However, immunity from external interfering radiation is dependent on careful wiring techniques. The accepted method is to use screened cables for all connections and to radially terminate the cable screens, in an appropriate grounded cable gland, at the point of entry into the industrial steel enclosure. If this is not possible, chassis ground screw terminals are provided on the G122-829A001. Exposed wires should be kept to a minimum length. Connect the screens at both ends of the cable to chassis ground.

## 4 Power supply

24 V DC nominal, 22 to 28 V
$75 \mathrm{~mA} @ 24 \mathrm{~V}$ without a load, 200mA @ 100 mA load.
If an unregulated supply is used the bottom of the ripple waveform is not to fall below 22 V .

It is recommended that an M205, 250mA T (slow blow) fuse, compliant with IEC 127-2 sheet 3, be placed in series with the +24 V input to protect the electronic circuit. If terminal 23 is used to power a proportional valve, the fuse should be increased to cater for the extra current.

## Caution

If you intend to use the feedback amplifier adjusted for 4-20mA, don't change the feedback gain or zero.

- They are already adjusted for $4-20 \mathrm{~mA}$
- To re-adjust for $4-20 \mathrm{~mA}$ takes a little time, needs test equipment and is tedious to do in the field.


## 6 Input configuration

Inputs 1, 2 and feedback go to the error amplifier and can be used for feedback or command. Care needs to be taken in selecting signal polarity to achieve negative feedback for the overall closed loop. Since the input error amplifier sums the signals, the transducer feedback signal needs to be the opposite polarity of the command. This can be achieved in two ways:
■ Arrange for an opposite polarity feedback transducer signal and connect it to input 1, input 2 or the positive feedback amplifier input.

- If the feedback transducer signal is the same polarity as the command, you only have one option: Connect it to the negative input of the feedback amplifier.


### 6.1 Feedback input

An input to the error amplifier: The feedback amplifier is the best choice for the feedback signal, for six reasons:
■ It leaves input 1 available for command. See 6.2 below.

- It has inverting (negative) and non-inverting (positive) inputs.
- It has zero and gain adjustment pots. This enables a signal that does not go to zero volts and has less span than the command, to be scaled up to the command. While this is not essential, it helps when setting up and trouble-shooting.
■ There is a front panel test point for the zeroed and amplified signal. This is very convenient (essential) for setting up and trouble-shooting.
- There is the option of a plug-in resistor, R16, to give a feedback derivative (lead or D) in the output of the feedback amplifier.
■ It can be set up for a current input by connecting a 240 Ohm resistor between terminals 17 and 18 with the $4-20 \mathrm{~mA}$ switch ([SW1:4]).


## Default

The feedback amplifier default set-up is $4-20 \mathrm{~mA}$ flowing into terminal 18 and out of terminal 17 , producing an output of 0 to -10 V . Reversing the terminals, and hence the current flow, will not result in a 0 to +10 V output. The feedback zero must be adjusted for this arrangement.

## Adjusting feedback amp for 4-20mA input and 0 to -10V output

- Set the feedback gain to minimum (fully counter clockwise). The trimpot has 15 turns and will click when minimum is reached.
- Connect terminal 17 to terminal 26 (ground).
- Connect the positive of a variable DC power supply to terminal 18 and the negative to terminal 26.
- Connect a digital multimeter (DMM), on DC Volts, between the front panel feedback amp and ground test points.
- Set the variable supply to 0.96 V .
- Adjust the feedback amp zero trimpot until the DMM reads 0.00 V .
- Set the variable supply to 4.80 V .
- Adjust the feedback gain trimpot until the DMM reads -10.00 V .
■ Set the variable supply to 0.96 V again and check the feedback test point is still 0.00 V . Trim if necessary and check the 4.80 V setting again.


### 6.2 Input 1

An input to the error amplifier: This input is $\pm 10 \mathrm{~V}$ non-inverting and has two important features:
■ It has a scale pot on its input that enables large inputs to be scaled down to match smaller signals on other inputs. Scale range is 10 to $100 \%$. Set fully clockwise (FCW), an input of 100 V can match a 10 V signal on the other inputs. Note that the maximum permissable input voltage is $\pm 95 \mathrm{~V}$.
■ It has a switch selectable (SW4:2) lag of 55 mS that can be used to remove transients from the input signal that could cause unwanted rapid movement in the output.
Input 1 is well suited to be a command because of these two features. If input 1 is used for feedback, be sure the lag is switched off. Input resistance after the scale pot is 94 k Ohms.

### 6.3 Input 2

An input to the error amplifier: This input is differential, with non-inverting and inverting inputs. It is switch selectable (SW5) between $4-20 \mathrm{~mA}$ and $\pm 10 \mathrm{~V}$. The $4-20 \mathrm{~mA}$ converter produces 0 to +10 V for 4 to 20 mA input to terminal 7. R34 connects from the output of the amplifier to the input of the error amp. It is a plug-in resistor with a default value of 100k Ohms, giving a nominal $\pm 10 \mathrm{~V}$ input signal range when V is selected. Input 2 is suitable for command or feedback. R34 can be increased to give a larger input range.
Terminal 8, the inverting input, can be connected to ground with SW6:1.

### 6.4 Input 3

An input to the output summing and limiting amplifier via a plug-in resistor, R33. A typical use for this input is command feed forward or closing the outer loop of a three stage valve. With R33 at 10 k Ohm, $\mathrm{a} \pm 10 \mathrm{~V}$ input will produce $\pm 100 \%$ valve drive. Increasing R33 reduces the valve drive.
The summing amp gain can be changed with plug-in resistor R27. This is useful if input 3 is being used to close the outer loop of a three stage valve.

## 7 Output configuration

Select the output to match the input requirements of the valve (SW2).

- When voltage ( V ) is selected, $\pm 10 \mathrm{~V}$ is available into a minimum load of 200 Ohm.
- When current (I) is selected, the current level switches (SW1:X) enable $\pm 5$ to $\pm 100 \mathrm{~mA}$ to be selected. The switch selections sum, so, if for instance 45 mA is required, select 30,10 and 5 . The output can drive all known Moog valves up to $\pm 100 \mathrm{~mA}$. The maximum load at I (Amp) output is:
RL max $=\left(\frac{11 \mathrm{~V}}{\mathrm{I}(\text { Amp })}-39\right) \mathrm{Ohm}$
eg. at 50 mA RL max is 181 Ohm
- When $4-20 \mathrm{~mA}$ is selected, the output V/I switches must be in I and the output current SW1 must have switch 3 selected for 20 mA . Maximum load for $4-20 \mathrm{~mA}$ output is 500 Ohm.
The output amplifier is limited to approximately 105\% of the selected full scale output. If both the proportional and integrator stages are saturated, the output will not be twice the selected full scale but still only $105 \%$ of full scale.


## 8 Step push button

The step push button (SW3) injects -50\% valve drive disturbance into the output. When released, the valve drive reverts to its original level. This feature is useful for closed loop gain optimisation.

## 9 P-I selection

For position closed loops, initially select only P (SW6:2). For pressure or velocity loops select I (SW6:4) initially and then P. See paragraph 12 below for more detail. For a complete discussion of P and I control, see the G122-202 servoamplifier Application Notes (part no C31015).

## 10 Integrator input

The servoamplifier has a unity gain input error amplifier followed by two parallel stages, one a proportional amplifier and the other an integrator. The outputs of these two stages can be switched to the output power amplifier (see paragraph 7 above) which then drives the valve.

The input to the integrator stage can be switch selected (SW4:1) from either the output of the error amplifier, I in = E, or the output of the proportional stage, I in $=\mathrm{P}$. The latter arrangement is used in the G122-202. It is beyond the scope of these Application Notes to detail the benefits of each arrangement. If you have experience with the G122-202, I in = P would seem to be an easy choice.

## 11 P only gain

For position loops select only P control (SW6:2). Input a step disturbance of $50 \%$ valve current with the step push button (SW3). Adjust the P gain for the required stability, while monitoring the front panel valve test point, or the feedback signal. The gain range of the proportional amplifier can be moved by changing the plug-in resistor R17. The value loaded when shipped is 100 k Ohms, which gives a 1 to 20 range. Selecting 200k Ohms will give 2 to 40. The circuit will function correctly with the value of R17 between 100k Ohms and 10M Ohms.
Note that as P gain is increased, the movement due to the step push button decreases.

## 12 P and I gains together

If you are inexperienced with integral control the following set-up method is a good starting point.
■ I in = E: Initially select only I (SW6:4). Press the step push button (SW3). Increase I gain until one overshoot in the feedback signal is observed.

Next select P (SW6:2) and I (SW6:4) together and increase the $P$ gain to reduce the overshoot.
For the I in = E arrangement the $P$ and $I$ sequence could be reversed. i.e.: adjust P first, followed by I.
■ I in = P: For an I in = P arrangement, only the "P followed by I" sequence of adjustment can be used.

For a more thorough discussion see G122-202 Application
Notes (part no C31015).

## 13 I limit

The contribution from the integrator to the output amplifier can be reduced by selecting I limit on (SW6:3). When this switch is on the integrator contribution is reduced to approximately $15 \%$ of the level when it is off. This feature is useful in a position loop that may require integral control to achieve the required steady state accuracy. The limited integral control removes valve null error when the final position is reached. It is also useful in a pressure loop to limit overshoot, if the valve drive saturates.

## 14 Dither

The dither frequency is fixed at 200 Hz and the level is adjustable with the front panel pot to $\pm 10 \%$ of valve drive, regardless of the type and level of valve drive selected. It can be turned on or off with ([SW1:3]). Dither is seldom needed in a position loop but can be beneficial in pressure or velocity loops. Increase dither until it can just be detected in the controlled variable, such as pressure or velocity. Dither can compromise valve life, so it should be kept to a minimum.

## 15 Enable

A relay on the circuit card needs to be energised to connect the output stage to its screw terminal and to un-clamp the integrator. The clamp prevents integrator wind-up when the loop is not operating. Supply 24 V to the appropriate terminal to energise the relay. The enable switch ([SW1:2]) on the circuit card can be set to permanently energise the relay and provide a permanent enable.

## 16 In position

When the valve drive signal falls below $\pm 10 \%$ of the selected full scale signal, the "in position" signal goes true and provides an opto-isolated current path between the + and - terminals. This can be connected to a PLC to initiate the next step in a control sequence. Do not apply more than 40 V to the + terminal and ensure the load on the - terminal is less than 20 mA .

The "in position" signal is not relevant for a velocity loop.

## 17 Withdrawing the circuit card from its case

The circuit card needs to be withdrawn from its case to set the selector switches, change the plug-in resistors and operate the step push button.

To do this, push one cover release tab with a pen or screwdriver, while gently pulling on the top cover on that side. The cover will release approximately one mm . Repeat on the second tab on that side. Repeat on the other side and then withdraw the cover and circuit card until the required switches are exposed. The rigidity of the connecting wires will hold the circuit card in position while changes are made.

## 18 Specifications

| Function: | P, I, or P \& I, switch selectable. |
| :---: | :---: |
| Input 1: | Connects to error amp via 94k. Scaled to 95V max with switch selectable lag of 55 mS . |
| Input 2: | Differential $4-20 \mathrm{~mA}$ or $\pm 10 \mathrm{~V}$, <br> switch selectable. <br> Connects to error amp via R34. <br> $\pm 15 \mathrm{~V}$ max. <br> Rin $=390 \mathrm{k}- \pm 10 \mathrm{~V}$. <br> $R$ in $=240 \mathrm{R}-4-20 \mathrm{~mA}$. <br> R34 is plug-in, 100K (default). |
| Input 3: | Connects to summing amp via R33. R33 plug-in. $\pm 10 \mathrm{~V}$ gives $\pm 100 \%$ valve drive when R33 $=10 \mathrm{k}$ Ohm, $\pm 10 \%$ when $R 33=100 \mathrm{k}$ Ohm. |
| Feedback input: | Differential $4-20 \mathrm{~mA}$ or $\pm 10 \mathrm{~V}$, <br> switch selectable. <br> $\pm 15 \mathrm{~V}$ max. <br> R in $100 \mathrm{k}- \pm 10 \mathrm{~V}$. <br> Rin 240R - 4-20mA. |
| Feedback amp: | ```Zero, }\pm10\textrm{V} Gain, 1 to 10. Derivative (velocity) feedback via plug-in resistor R16 and fixed capacitor.``` |
| Transducer excitation: | +10V @ 10mA max. |
| Error amp: | Unity gain. $\text { Bias } \pm 1.5 \mathrm{~V} \text {. }$ |
| Proportional amp gain: | 1 to 20 with R17 = 100k (default). Max gain 2000 with R17 = 10M. |
| Integrator gain: | 1 to 45 per second. |
| Integrator input: | Switch selectable from output of unity gain error amp or proportional gain amp. |
| Enable: | Relay, +24V @ 8mA, 17 to 32V. |
| Output amp: | Switch selectable voltage, current or 4-20mA, single ended output, return to ground. <br> $\mathrm{V} . \pm 10 \mathrm{~V}$, minimum load $=200 \mathrm{Ohm}$. <br> I. $\pm 5,10,20,30,50 \mathrm{~mA}$ to a maximum of $\pm 100 \mathrm{~mA}$. <br> max load $=\left(\frac{11 \mathrm{~V}}{I(\mathrm{Amp})}-39\right)$ Ohm <br> 4-20mA. Max load 500R. |
| Step push button: | -50\% valve drive disturbance. |
| Valve supply: | Terminal 23, 300mA max. |
| In position: | $\pm 10 \%$ of valve drive. 20 mA and 40 V max output to PLC. |
| Front panel indicators: | Vs, internal supply - green <br> Valve drive positive - red negative - green |
|  | Enable - yellow In position - green |
| Front panel test points: | Valve $\pm 10 \mathrm{~V}$ (regardless of output signal selection) Feedback amplifier output signal OV |
| Front panel trimpots: (15 turns) | Input 1 scale <br> Error amp bias <br> P gain <br> I gain <br> Dither level <br> Feedback amp gain <br> Feedback amp zero |


| Dither: | 200 Hz fixed frequency. <br> $\pm 10 \%$ valve drive. Switch selectable on/off. |
| :---: | :---: |
| Supply: | Terminal 1, <br> 24 V nominal, 22 to 28 V <br> $75 \mathrm{~mA} @ 24 \mathrm{~V}$, no valve current, <br> 200mA @ 100mA valve current. |
| $\pm 15 \mathrm{~V}$ output: | Terminals 14 and 15, $\pm$ ( 110 mA - max valve current). |
| Wire size range: | $\begin{aligned} & 0.2 \mathrm{~mm}^{2} \text { to } 2.5 \mathrm{~mm}^{2} \\ & \text { (24AWG to } 12 \mathrm{AWG}) . \end{aligned}$ |
| Recommended supply protection: | M205, 250mA T (slow blow) fuse compliant to IEC127-2 sheet 3. If terminal 23 is used to power a proportional valve, the fuse should be increased to cater for the extra current. |
| Mounting: | $\begin{aligned} & \text { DIN rail } \\ & \text { IP } 20 \end{aligned}$ |
| Temperature: | 0 to $+40^{\circ} \mathrm{C}$ |
| Dimensions: | $100 \mathrm{~W} \times 108 \mathrm{H} \times 45 \mathrm{D}$ |
| Weight: | 180 g |
| CE mark: | EN50081.1 emission EN61000-6-2 immunity |
| C tick: | AS4251.1 emission |

## 19 Internet

www.moog.com/dinmodules


Industrial Controls Division. Moog Inc., East Aurora, NY 14052-0018. Telephone: 716/652-3000. Fax: 716/655-1803. Toll Free 1-800-272-MOOG Moog GmbH. Germany. Telephone: 07031-622-0. Fax: 07031-622-100
Moog Sarl. France. Telephone: 01456070 00. Fax: 0145607001.
Moog Australia Pty. Ltd. Telephone: 039561 6044. Fax: 0395620246.
Moog pursues a policy of continuous development and reserves the right to alter designs and specifications without prior notice. Information contained herein is for guidance only and does not form part of a contract.

